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## Uncertainty evaluation of humidity sensors calibrated by saturated salt solutions

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### Abstract

This study evaluates the sources of uncertainty for two types of humidity sensors. The standard humidity environment was made by several saturated salt solutions. These uncertainty sources include predicted values of calibration equation, reference humidity source, temperature variation effect, nonlinear and repeatability, and resolution source. The study also dealt with the effect of calibration methods and calibration equations on the uncertainty. The polynomial calibration equation had better predictive performance than the linear equation for two types of humidity sensors.

The uncertainty analysis shows that the predicted uncertainty is the main source for combined uncertainty. No significant difference of the uncertainty for resistive sensor was found between classical method and inverse method. However, the predicted uncertainty of inverse method is significantly lower than that of classical method for capacitive humidity sensor.

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*Keywords:* Humidity sensor; Uncertainty; Calibration

### 1. Introduction

Humidity is an important factor that affects the quality of foodstuffs, the growth of microorganisms, and the package process of microelectric [1]. The accuracy and precision of the humidity measurement have been considered for various industries. Two types of electrical humidity sensors: capacitive and resistive type, are widely used in commercial, industrial, and weather stations. The uncertainty of these humidity sensors is a concerned of users.

They are four-types humidity standard generator systems: two-pressure humidity generator [1], two-temperature humidity generator [2], divided-flow humidity generator [3,4], and fixed-point humidity systems [5]. Except for the fixed-point humidity systems, others can provide more accurate standard environment [1]. However, they are expensive and complicated. Sometimes, an experimental factory needs to be established to install these systems.

The fixed relative humidity point certified with saturated salt solutions is easy to be made [5]. A number of fixed relative humidity points could serve as the secondary standards for the calibration of humidity sensors. This fixed points method is inexpensive, convenient, and easy to be reproduced in

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46 a research laboratory. It is often used for the check-  
47 ing points for humidity sensors. However, the fixed  
48 values of humidity environment limit the applicable  
49 range of sensors. As the humidity sensor was  
50 checked at two fixed points, the accuracy and uncer-  
51 tainty of the measuring points between two check-  
52 ing points cannot be determined directly.

53 Recently, uncertainty evaluation had been widely  
54 adopted for sensors [6–8]. The accuracy uncertainty  
55 analysis is very useful. In this study, two types of  
56 electrical humidity sensors are calibrated by several  
57 saturated salt solutions. The adequate calibration  
58 equations are evaluated. The build of calibration  
59 equation is analyzed. According to ISO GUM [9],  
60 the uncertainty of two humidity sensors was evalu-  
61 ated by all sources of uncertainty.

## 62 2. Equipment and methods

### 63 2.1. Humidity sensors

64 Two types of humidity sensors were adopted in  
65 this study. They are resistive humidity sensor and  
66 capacitive humidity sensor. The specifications of  
67 these sensors are listed in Table 1.

### 68 2.2. Saturated salts solutions

69 The fixed humidity environments produced by 10  
70 saturated salt solutions were used to calibrate two  
71 types of humidity sensors. These saturated salt  
72 solutions are listed in Table 2. The procedure for prepar-  
73 ing a hydrostatic solution was according to the  
74 OIML R121 [10]. The purity of salt was 99.99%.  
75 The distilled water was selected as solvent. The salt  
76 was dissolved in water in such a proportion that 30–  
77 90% of the weighted sample remained as dissolved.

78 These salt solutions were placed in a vessel. Then  
79 these vessels were installed in a temperature control-  
80 ler. The ambient air temperature was set at 25 °C  
81 and the variation of air temperature was kept within  
82 0.2 °C.

Table 2

The saturated salt solution and its standard relative humidity value for the calibration of humidity sensors at 25 °C

Salt solutions	Standard relative humidity (%)	Uncertainty (%)
LiCl	11.3	0.3
CH <sub>3</sub> COOK	22.5	0.4
MgCl <sub>2</sub> · 6H <sub>2</sub> O	32.8	0.2
K <sub>2</sub> CO <sub>3</sub>	43.2	0.4
NaBr	57.6	0.4
KI	68.9	0.3
NaCl	75.3	0.2
KCl	84.3	0.3
KNO <sub>3</sub>	93.6	0.55
K <sub>2</sub> SO <sub>4</sub>	97.3	0.5

Source: Greenspan [5].

At the calibrating process, each humidity sensor 83  
was placed at the headspace of the vessel with the 84  
saturated salt solutions. The calibrating period 85  
was maintained 12 h to ensure the internal air 86  
humidity would reach the equilibrate state. 87

### 2.3. Establish the calibration equation 88

The work of calibration equation is to establish 89  
the relationship between the reading values of sen- 90  
sor and the standard values of humidity. In this 91  
study, the standard humidity environments, the 92  
known  $x_i$  values, were maintained by saturated salt 93  
solutions. The reading values, the response  $y_i$ , were 94  
taken from humidity sensor. There are two mathe- 95  
matical ways to build the calibration equations. 96

#### (A) The classical method 97

The response  $y_i$  was the function of standard  $x_i$  98  
values: 99

$$y = f(x_i) \quad (1) \quad 101$$

If  $y_i$  and  $x_i$  was a linear relationship, then 102

$$y = b_0 + b_1x \quad (2) \quad 104$$

As the new response,  $x_0$ , was measured, the “true” 105  
value is estimated as 106

Table 1  
Specifications of the humidity sensors

	Resistive humidity sensor	Capacitive humidity sensor
Sensing element	Macro-molecule resistive element	Capacitive-type
Measuring range	0–99% RH	0–100% RH
Nonlinearity and repeatability	±0.25% RH	±0.1% RH
Resolution	0.1% RH	0.2% RH
Temperature shift	Not available	0.005%/°C (deviated with 20 °C)

$$\hat{x} = \frac{\hat{y} - b_0}{b_1} \quad (3)$$

This procedure is known as the classical method to calibration. If the relationship between  $y_i$  and  $x_i$  was nonlinear or polynomial function, the true values ( $\hat{x}$ ) of measured values ( $\hat{y}$ ) then be calculated as an algebra equation or computed by numeric analysis technique. The calibration equation was built by ordinary least square regression or nonlinear regression technique.

(B) The inverse method

In this case, the  $x_i$  is selected as dependent variable and  $y_i$  is viewed as independent variable, the calibration equation is:

$$x = g(y) \quad (4)$$

As  $y_i$  and  $x_i$  had the linear relationship:

$$x = c_0 + c_1 y_i \quad (5)$$

The true value  $\hat{x}$  then can be calculated directly by Eq. (5).

The  $g(y)$  can be a polynomial function or nonlinear equation, such as:

$$x = c_0 + c_1 y + c_2 y^2 \quad (6)$$

or

$$x = c_0 \text{Exp}(c_1 y + c_2 y^2) \quad (7)$$

This approach is called the inverse method.

Many textbooks of regression analysis only mentioned the classical method. Krutchkoff first reported the inverse method [11]. The author mentioned that inverse method had the smaller mean squared error  $b$  than that of classical method. After comparing the accuracy of predictions from classical and inverse method, Krutchkoff [11] concluded that the inverse method was better than classical method for prediction. Centner et al. [12] verified this statement by Monte Carlo simulations and two practical cases, their conclusion showed that the classical method gave more reliable predictions than classical method. Tellinghuisen [13] had the similar results when comparing two approach calibration methods with small data sets. Grientschnig [14] confirmed that inverse method had the better predict ability than classical method regardless of the size of the data sets.

#### 2.4. Criteria for model evaluation

The relationships between reading values of sensor and standard humidity values are calculated by

Sigma plot version 6.0. The standard error of the estimated value,  $s$ , was selected as the quantitative criteria:

$$s = \sqrt{\frac{(y - \hat{y})^2}{n - 1}} \quad (8)$$

where  $y$  is the dependent variable,  $\hat{y}$  is the predicted value of model, and  $n$  is the number of data.

The relationship between residuals of model and the predicted values are plot as residual plots. For an adequate model, data distribution of residual plots should tend to be in a horizontal band centered on zero. If the residual plots indicated a clear pattern, the model could not be accepted.

### 3. Sources of the uncertainty for humidity sensors

According to the ISO GUM [9], the uncertainty of measurement is evaluated by a 'Type A' or 'Type B' method. The Type A evaluation of standard uncertainty is the method of evaluation by the statistical analysis of observations. The Type B evaluation of standard uncertainty is the method of evaluation by other information about the measurement.

There are several uncertainty source items. The uncertainties were calculated as follows.

#### 3.1. The calibration equation

The standard uncertainty due to calibration equation is a Type A uncertainty. In this study, two calibration methods are considered.

(A) The classical method

(a) Linear equation

The form of linear regression equation is:

$$y = b_0 + b_1 x \quad (9)$$

where  $y$  is the reading values of humidity sensor and  $x$  is the standard value. The predicted value ( $x_{\text{pred}}$ ) that calculated from the observed response ( $y_{\text{obs}}$ ) has been discussed in detail [15–17]:

$$x_{\text{pred}} = \frac{y_{\text{obs}} - b_0}{b_1} \quad (10)$$

The variance of  $x_{\text{pred}}$  is given:

$$\text{Var}(x_{\text{pred}}) = \frac{s^2}{b_1^2} \left[ \frac{1}{p} + \frac{1}{n} + \left[ \sqrt{\frac{(x_{\text{pred}} - \bar{x})^2}{\sum(x_i^2) - (\sum x_i)^2/n}} \right] \right] \quad (11)$$

201 where  $s$  is the standard deviation of calibration  
 202 equation,  $p$  is the numbers of measurement for pre-  
 203 diction,  $n$  is total number of measurement for cali-  
 204 bration equation.

205 The standard deviation  $s(y_c)$  for a value of  $y$  cal-  
 206 culated from the fitted line for new value of  $x$ :  
 207

$$209 \quad s(y_c) = s \sqrt{\frac{1}{p} + \frac{1}{n} + \frac{(x_{\text{pred}} - \bar{x})^2}{\sum(x_i^2) - (\sum x_i)^2/n}} \quad (12)$$

210 Combining Eqs. (11) and (12):

$$212 \quad \text{Var}(x_{\text{pred}}) = \left[ \frac{s(y_c)}{b_1} \right]^2 \quad (13)$$

213 then  
 214

$$216 \quad u(x_{\text{pred}}) = \frac{s(y_c)}{b_1} \quad (14)$$

217 The uncertainty of predicted values obtained by  
 218 inverse method of the linear calibration equation  
 219 could be computed by Eq. (14).

220 (b) Polynomial equation

221 The form of polynomial equation is:

$$223 \quad y = c_0 + c_1x + c_2x^2 \quad (15)$$

224 The predicted value ( $x_{\text{pred}}$ ) calculated from the  
 225 observed response ( $y_{\text{obs}}$ ) is calculated as:

$$227 \quad x_{\text{pred}} = \frac{-c_1}{2c_2} + \sqrt{\frac{c_1^2}{4c_2^2} - \frac{c_0}{c_2} + \frac{y_{\text{obs}}}{c_2}} \quad (16)$$

228 From the definition of uncertainty:

$$u(x_{\text{pred}}) = \frac{\delta x}{\delta y} u(y_i) \quad (17)$$

$$230 \quad u(x_{\text{pred}}) = \frac{1}{2c_2} \frac{u(y_{\text{obs}})}{\sqrt{\frac{c_1^2}{4c_2^2} - \frac{c_0}{c_2} + \frac{y_{\text{obs}}}{c_2}}} \quad (18)$$

231  $u(y_{\text{obs}})$  can be calculated by Eq. (12).

232 (B) The inverse method

233 (a) Linear equation

234 The form of linear regression model is:

$$236 \quad x = d_0 + d_1y. \quad (19)$$

237 (b) Polynomial equation

238 The form of polynomial equation is:

$$240 \quad x = e_0 + e_1y + e_2y^2 \quad (20)$$

241 The uncertainty of  $x_{\text{pred}}$  is easy to be calculated  
 242 by the following equation:

$$u(x) = s(x_c) = s \sqrt{\frac{1}{p} + \frac{1}{n} + \frac{(y - \bar{y})^2}{\sum(y_i^2) - (\sum y_i)^2/n}}. \quad (21) \quad 244$$

### 3.2. Uncertainty of the reference standard 245

The reference standard of humidity is made by 246  
 saturated salt solutions. The scale and the uncer- 247  
 tainty of these reference standards is provided by 248  
 the Organization Internationale De Metrologie 249  
 Legale (OIML) R121 [10] and Greenspan [5]. The 250  
 distribution of uncertainty at two temperatures is 251  
 shown in Fig. 1. No distribution pattern could be 252  
 found. An approximate estimate of uncertainty for 253  
 the reference standard is to consider the average 254  
 value of uncertainty: 255  
 256

$$u_{\text{ref}} = \pm \frac{\sum U_{\text{ref}}}{N_2} \quad (22) \quad 258$$

where  $U_{\text{ref}}$  is the uncertainty of humidity made by 259  
 saturated salt solutions and  $N_2$  is the number of sat- 260  
 urated salt solutions for calibration. 261

### 3.3. Uncertainty due to temperature variation 262

The calibration of humidity sensors is performed 263  
 in standard laboratory environment. Where the 264  
 temperature is maintained within  $25 \pm 0.2$  °C. The 265  
 variation response from the temperature variation 266  
 is assumed a rectangular distribution: 267  
 268

$$u_{\text{temp}} = \pm \frac{K_{\text{temp}} \Delta t}{\sqrt{3}} \quad (23) \quad 270$$

where  $K_{\text{temp}}$  is the temperature coefficient of sensi- 271  
 tivity per 1 °C. This numeric value is specified in 272  
 the manufacturer's manual.  $\Delta t$  is half of the ex- 273

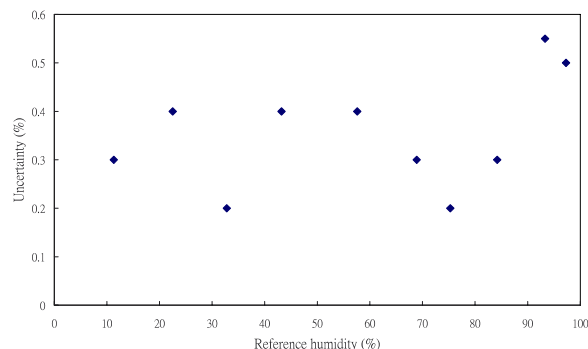


Fig. 1. The uncertainty vs. reference humidity made by saturated salt solutions at 2 °C.

274 pected temperature variations ranged during cali-  
275 bration period.

### 276 3.4. Uncertainty due to nonlinearity and repeatability

277 The deviation  $U_{\text{non}}$  due to nonlinearity and  
278 repeatability is specified by manufacturers. The vari-  
279 ation response for this error is assumed a rectangu-  
280 lar distribution. The uncertainty due to nonlinear  
281 and repeatability is calculated as:

$$284 u_{\text{non}} = \pm \frac{U_{\text{non}}}{2\sqrt{3}}. \quad (24)$$

### 285 3.5. Uncertainty due to resolution

286 The uncertainty measurement due to resolution is  
287 assumed a rectangular distribution. It is considered  
288 as  $\pm 1/2$  of the scale value of the display. The uncer-  
289 tainty value due to resolution ( $U_{\text{res}}$ ) is estimated as  
290 the follows:

$$293 u_{\text{res}} = \pm \frac{U_{\text{res}}}{2\sqrt{3}} \quad (25)$$

294 where  $U_{\text{res}}$  is the uncertainty due to the resolution  
295 effect.

### 296 3.6. Uncertainty due to hysteresis

297 The uncertainty measurement due to hysteresis  
298 did not be mentioned by manufacturers. Stevens  
299 et al. [18] compared the performance of several rela-  
300 tive humidity meters, the effect of hysteresis was  
301 insignificant. In this study, the uncertainty measure-  
302 ment due to hysteresis did not be considered.

303 The uncertainty due to the reference standard,  
304 temperature variation, nonlinear and repeatability,  
305 and resolution are classified as Type B uncertainty.

## 306 4. Calculation of the uncertainty of humidity sensor

### 307 4.1. Resistive humidity sensor

308 The relationship between reading values of resis-  
309 tive humidity sensor and the standard humidity  
310 environment made by saturated salt solutions are  
311 presented in Fig. 2. The calibration equations with  
312 different methods are introduced as follows.

#### 313 (A) Classical method

314 In this equation, the standard humidity values  
315 serve the independent variables ( $x$ ), and the reading  
316 values of resistive humidity sensors are the depen-

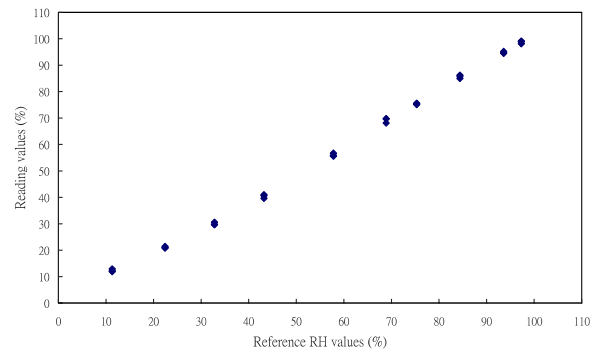


Fig. 2. Relationship between reading values and standard relative humidity values made by saturated salt solutions for resistive humidity sensor.

317 dent variables ( $y$ ). The calibration equation is calcu-  
318 lated by regression analysis.

(a) Linear equation 319

$$321 y = -0.572 + 1.00583x \quad (26)$$

$$321 R^2 = 0.9967, \quad s = 1.836$$

For the  $x_{\text{pred}}$ : 322

$$322 x_{\text{pred}} = (y_{\text{obs}} + 0.572)/1.00583 \quad (27)$$

$$325 u(x_{\text{pred}}) = s(y_c)/1.00583 \quad (28)$$

326 As new observed variable of  $y$  is 30% RH, the  
327 predicted value of  $x$  is 30.395%,  $s(y_c) = 1.8795\%$ ,  
328 so the  $u(x_{\text{pred}}) = 1.8686$ . The values of  $x_{\text{pred}}$  and  
329  $u(x_{\text{pred}})$  for observation of 60% RH and 90% RH  
330 can be calculated by Eqs. (27) and (28).

331 The residual plot of this linear equation is shown  
332 in Fig. 3. A systematic pattern is found. In spite of  
333 the high  $R^2$  value, the results of the residual plots  
334 indicated that the linear calibration equation could  
335 not be recognized as an adequate model.

(b) Polynomial equation 336

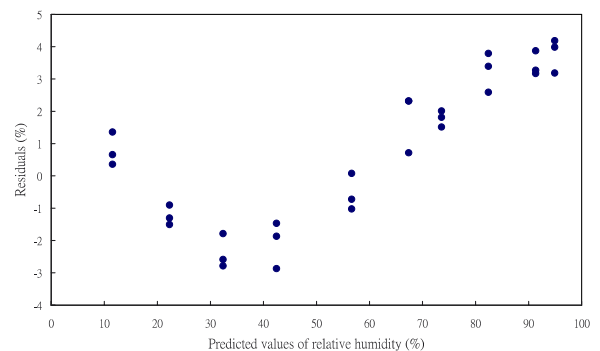


Fig. 3. Residuals plots for classical linear equation for resistive humidity sensor.

Table 3  
The predicted values and uncertainty of three observations for resistive humidity sensor for two types of calibration equations

Calibration method	Regression equation	$y_{obs}$					
		30% RH		60% RH		90% RH	
		$x_{pred}$	$u(x)$	$x_{pred}$	$u(x)$	$x_{pred}$	$u(x)$
Classical	Linear	30.39	1.8686	60.22	1.8508	90.05	1.8805
	Polynomial	31.46	1.1954	61.88	1.1541	89.22	1.1511
Inverse	Linear	31.31	1.5641	60.51	1.5411	89.69	1.5644
	Polynomial	31.59	1.1843	61.77	1.1926	89.21	1.1865

337 The result for the polynomial calibration equation is shown as follows:

338 
$$y = 2.7637 + 0.8047x + 1.9409 \times 10^{-3}x^2$$

340 
$$R^2 = 0.9987, \quad s = 1.1656$$

341 For the  $x_{pred}$ :

342 
$$x_{pred} = \frac{-0.8047 + \sqrt{22.1037 - 7.7636y}}{3.8818}$$

343 
$$u(x_{pred}) = \frac{257.6u(y_{obs})}{\sqrt{4.545 + 515.2y_{obs}}}$$

344 The  $x_{pred}$  and  $u(x_{pred})$  for three observations: 30%,  
345 60% and 90% are listed in Table 3.

346 The residual plot for this calibration equation is  
347 shown in Fig. 4. The uniform distribution of the  
348 scattered points indicated the equation was  
349 adequate.

350 (B) Inverse method

351 For the inverse calibration equation, the reading  
352 values of resistive humidity sensors are the independent  
353 variable ( $y$ ), and the standard humidity values  
354 are the dependent variables ( $x$ ). The calibration  
355 equations were conducted.

356 (a) Linear equation

$$x = 2.1143 + 0.9731y$$

$$R^2 = 0.9973, \quad s = 1.517$$

The residual plot of this equation indicated a clear  
pattern.

(b) Polynomial equation

The results for the equation were:

$$x = -1.3568 + 1.1439y - 1.5294 \times 10^{-3}y^2$$

$$R^2 = 0.9985, \quad s = 1.1147$$

The  $x_{pred}$  and  $u(y_{pred})$  for three observations are  
listed in Table 3. The residual plots for this polynomial  
equation indicated a uniform distribution.

The Type B uncertainty analysis for resistive  
humidity sensor is calculated by Eqs. (22), (24)  
and (25). The result is listed in Table 4.

4.2. Capacitive humidity sensor

The relationship between reading values of  
capacitive humidity sensor and the standard humidity  
environment from saturated salt solutions is  
shown in Fig. 5.

(A) Classical method

The calibration equation is:

(a) Linear equation

$$y = -0.2521 + 0.9705x$$

$$R^2 = 0.9983, \quad s = 1.1187.$$

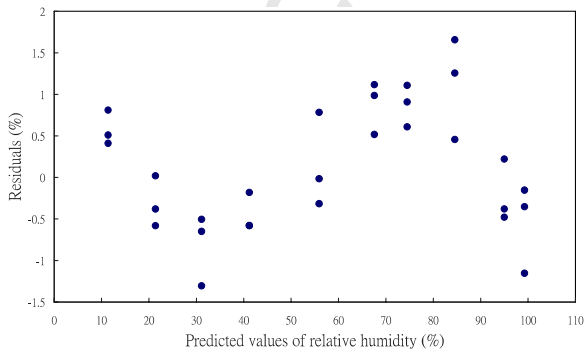


Fig. 4. Residuals plots for classical polynomial equation for resistive humidity sensor.

Table 4  
The Type B uncertainty analysis for resistive humidity sensor

Description	Estimate value (%)	Standard uncertainty $u(x)$ (%)	Probability distribution
Reference standard, $U_{ref}$	$\pm 0.3333$	0.1924	Rectangular
Nonlinear and repeatability, $U_{non}$	$\pm 0.25$	0.0072	Rectangular
Resolution, $U_{res}$	0.1	0.0029	Rectangular

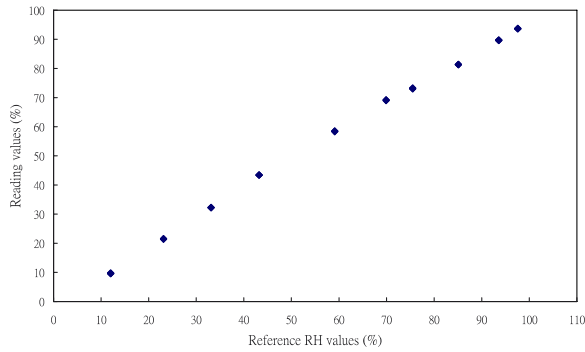


Fig. 5. Relationship between reading values and standard relative humidity values made by saturated salt solutions for capacitive humidity sensor.

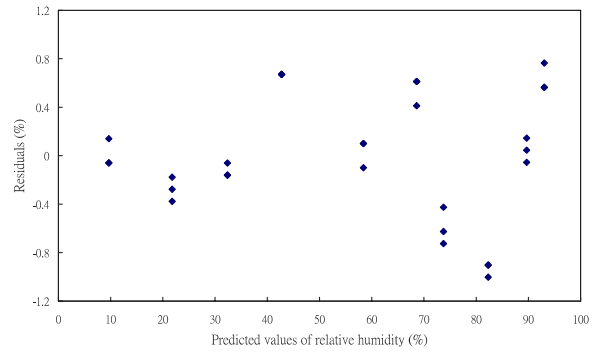


Fig. 7. Residual plots for classical polynomial equation for capacitive humidity sensor of classic polynomial equation.

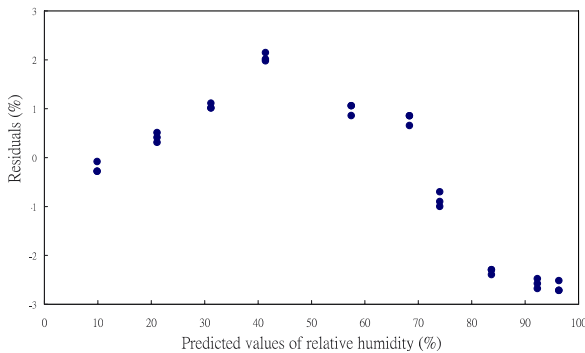


Fig. 6. Residuals plots for classical linear equation for capacitive humidity sensor.

381 The residual plot is presented in Fig. 6. The clear  
382 pattern indicated the linear equation could not be  
383 recognized as an adequate model:

$$x_{\text{pred}} = (y_{\text{obs}} + 0.2521)/0.9705 \quad (35)$$

385  $u(x_{\text{pred}}) = s(y_c)/b_1 \quad (36)$

386 The predicted values and uncertainty is listed in  
387 Table 5.

388 (b) Polynomial equation

$$y = -3.877 + 1.1471x - 1.5791 \times 10^{-3}x^2 \quad (37)$$

390  $R^2 = 0.9997, \quad s = 0.5311$

The residual plots (Fig. 7) showed a systematic 391  
pattern and indication the fitting-agreement of this 392  
model: 393

$$u(x) = \frac{316.64u(y_{\text{obs}})}{\sqrt{15654 + 633.3y}} \quad (38) \quad 395$$

The predicted values and uncertainty is listed in 396  
Table 5. 397

(B) Inverse method 398

(a) Linear equation 399

$$x = 0.36025 + 1.0286y \quad (39) \quad 401$$

$$R^2 = 0.9983, \quad s = 1.222.$$

(b) Polynomial equation 402

$$x = 3.7345 + 0.8498y + 1.6942 \times 10^{-3}y^2 \quad (40) \quad 404$$

$$R^2 = 0.9997, \quad s = 0.552$$

The predicted values and uncertainty is listed in 405  
Table 5. 406

The Type B uncertainty analysis for capacitive 407  
humidity sensor is calculated by Eqs. (22)–(25). This 408  
result is listed in Table 6. 409

Table 5

The predicted values and uncertainty of three observations for capacitive humidity sensor for two kinds of calibration equations

Calibration method	Regression equation	$y_{\text{obs}}$					
		30% RH		60% RH		90% RH	
		$x_{\text{pred}}$	$u(x)$	$x_{\text{pred}}$	$u(x)$	$x_{\text{pred}}$	$u(x)$
Classical	Linear	31.17	1.2641	62.08	1.2434	92.99	1.2664
	Polynomial	30.75	0.9354	60.82	1.1343	93.94	1.1663
Inverse	Linear	31.22	1.2611	62.08	1.2425	92.93	1.2699
	Polynomial	30.95	0.571	60.77	0.5736	93.88	0.5815

Table 6  
The Type B uncertainty analysis for the capacitive humidity sensor

Description	Estimate value (%)	Standard uncertainty $u(x)$ (%)	Probability distribution
Reference standard, $U_{\text{ref}}$	$\pm 0.3333$	0.1924	Rectangular
Temperature, $U_{\text{temp}}$	$\pm 0.0075$	0.0043	Rectangular
Nonlinear and repeatability, $U_{\text{non}}$	$\pm 0.1$	0.0058	Rectangular
Resolution, $U_{\text{res}}$	0.2	0.0058	Rectangular

#### 4.3. The combined standard uncertainty ( $u_c$ )

Comparing these sources of uncertainty for resistive humidity sensor with Tables 3 and 4, the main source of the uncertainty is from the predicted uncertainty. The uncertainty of polynomial equation is significantly less than that of linear equation for classical or inverse method for resistive humidity sensor. The comparison of the source of uncertainty for capacitive humidity sensor with Tables 5 and 6 also had similar results.

The combined standard uncertainty ( $u_c$ ) can be estimated from the following equation:

$$u_c = \sqrt{\sum u_i^2} = \sqrt{u_{\text{ref}}^2 + u_{\text{temp}}^2 + u_{\text{non}}^2 + u_{\text{res}}^2 + u^2 X_{\text{pred}}} \quad (41)$$

The  $u_c$  value for two humidity sensors used two calibration equations at three observations are listed in Table 7.

According to Eq. (41), the values of  $u_c$  are calculated at 30%, 60% and 90% of the observed humidity. They are found to be 1.8785%, 1.8608%, and 1.8904% for resistive humidity sensor using linear classical calibration equation, respectively. For the polynomial form of calibration equation, the combining standard uncertainty evaluated at 30%, 60% and 90% of the relative humidity were 1.2108%, 1.1701% and 1.1816%, respectively. The linear equa-

tion is an inadequate equation by the display of residual plots. This result indicated that the inadequate calibration equation could increase the uncertainty significantly. A similar result also was found for the inverse method and for two calibration methods of the capacitive humidity sensor.

Comparing the combined standard uncertainty of the polynomial equations between the classical model and inverse model for observation values of 30%, 60% and 90% RH, both sets of data did not have a significant difference for resistive humidity sensor.

The values of  $u_c$  obtained at 30%, 60% and 90% of the observed humidity for the capacitive humidity sensor had different results. The  $u_c$  values of the linear equation are higher than that of polynomial equation for classical and inverse method. The combined uncertainty calculated by calibration equations of the classical method is significantly higher than that of inverse method.

The uncertainty arising from the inadequate calibration equation has been mentioned [19]. The methods of calibrating  $u(x)$  due to the addition variation of inadequate equation are proposed in this study. The adding variation of inadequate equation is found as the main source of uncertainty.

The uncertainty analysis has become the basis information for sensors. No literature was found that mentioned the calculation of uncertainty analysis of electrical humidity sensors. In this study,

Table 7  
The combined standard uncertainty for two humidity sensors

Humidity Sensor	Calibration method	Regression equation	Observations		
			30% RH	60% RH	90% RH
Resistive	Classical	Linear	1.8785	1.8608	1.8904
		Polynomial	1.2108	1.1701	1.1816
	Inverse	Linear	1.5759	1.5531	1.5762
		Polynomial	1.1999	1.2080	1.2020
Capacitive	Classical	Linear	1.2786	1.2582	1.2810
		Polynomial	0.9550	1.1505	1.1820
	Inverse	Linear	1.2756	1.2573	1.2844
		Polynomial	0.6026	0.6051	0.6126



467 the fixed relative humidity point was made by satu-  
 468 rated salt solutions. The novelty method of uncer-  
 469 tainty calculation was developed. This method was  
 470 easily applied in a research laboratory.

## 471 5. Conclusion

472 This study evaluated the sources of uncertainty  
 473 for two types of humidity sensors. These sources  
 474 include predicted values of calibration equation, ref-  
 475 erence source, temperature variation effect, nonlin-  
 476 ear and repeatability, and resolution source. The  
 477 study also dealt with the effect of calibration meth-  
 478 ods and calibration equations on the uncertainty.

479 The uncertainty analysis shows that the predicted  
 480 uncertainty is the main source for combined uncer-  
 481 tainty. No significant difference of the uncertainty  
 482 for resistive sensor was found between classical  
 483 method and inverse method. However, the predicted  
 484 uncertainty of inverse method is significantly lower  
 485 than that of classical method for capacitive humid-  
 486 ity sensor. For both humidity sensors, the adding  
 487 variation of inadequate equation is found as the  
 488 main source of uncertainty.

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